

Silent earthquakes occurring in a stable-unstable transition zone and implications for earthquake prediction

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In the past decade, nine silent earthquakes were documented along the Nankai and the Sagami Troughs in Japan, which form the northwestern margin of the Philippine Sea plate. They occurred in the stable-unstable transition zone at depths of around 30 km on the subduction interface and were segregated from major asperities of the 1923 Kanto, the 1944 Tonankai and the 1946 Nankai earthquakes. Their equivalent magnitudes were less than 7 and overall slips were less than 0.2 m, one-order smaller than those of the major asperities of ordinary great earthquakes. Moment release rates of the silent earthquakes were less than 10^{14} Nm/s, five-orders smaller than 10^{19} Nm/s of the great earthquakes. Two methodologies are attempted to obtain order of magnitude estimates of the roughness and friction parameter of source areas of some of the silent earthquakes. One method compares observed waveforms to synthetics with an empirical source time function based on laboratory experiment. The other relates sizes of silent earthquakes to the friction parameter $a-b$.

Key words: Silent earthquake, fault roughness, stable-unstable transition zone, Nankai Trough, Sagami Trough.

1. Introduction

Great M_w 8 earthquakes recur at intervals of about 100 years along the Nankai and the Sagami Troughs on the northwestern margin of the Philippine Sea plate, which is subducting at a rate of around 5–6 cm/yr (e.g., Seno *et al.*, 1993). Figure 1 shows a vertical cross section of the distribution of microearthquakes (Nakamura *et al.*, 1997) under southwest Japan. The region labeled (A) is the seismogenic zone where the interplate coupling is strong and major earthquakes recur. (C) is a region where stable sliding is dominant. (B) is the stable-unstable transition zone between (A) and (C), as suggested by geodetic inversion of GPS data by Ito *et al.* (1999) and Sagiya (1999).

This article consists of two parts: a summary of silent earthquakes recently documented along the Nankai and the Sagami Troughs and two independent order of magnitude estimates of the roughness and friction parameter of the source areas of silent earthquakes on the subduction interface.

2. Spatial Distribution of Silent Earthquakes

There have previously been numerous studies on aseismic events: e.g., Pelayo and Wiens (1992) and Kanamori and Kikuchi (1993) from anomalous excitation of long period seismic waves, Beroza and Jordan (1990) from free oscillations and Linde *et al.* (1988) and Kawasaki *et al.* (1995) from continuous recordings of crustal strains and tilts. Recently, there were new findings of silent earthquakes with GPS data in the Cascadia (e.g., Dragert *et al.*, 2001), Alaskan (e.g., Freymueller *et al.*, 2002) and Mexican (e.g., Lowry *et al.*, 2001) subduction zones.

In Japan, there have been 9 silent earthquakes identified in the past decade along the Nankai and the Sagami Troughs, as listed in Table 1 and plotted together with ordinary great earthquakes in Fig. 2. Slow-slip-event is hereafter used as a general term for all aseismic events. M_{wa} is an equivalent magnitude of slow-slip events, first defined by Kawasaki *et al.* (2001) through a relationship, $\log Moa = 1.5M_{wa} + 9.1$, where Moa (Nm) is the static moment inverted from geodetic data.

Fujii (1993) obtained a fault plane solution and an interplate moment of the 1970 Chiba silent earthquake (SL1 in Table 1) by an inversion of leveling data from GSI (Geographical Survey Institute, Japan). The source duration time of the event is unknown. Hirose *et al.* (2000) found the 1989 Tokyo Bay silent earthquake (SL2) (M_{wa} 5.9) with a source duration time of around 1 day, using continuous recordings of crustal tilts by NIED (National Research Institute of Earth Sciences and Disaster Prevention, Japan). Other events were detected by GPS data of GEONET, which was established in 1994 by GSI (e.g., Hatanaka *et al.*, 2003). Sagiya (2004) obtained fault models of the offshore Boso Peninsula silent earthquakes that recurred in 1996 (M_{wa} 6, source duration time of a few days, SL3) and in 2002 (M_{wa} 6.5, source duration time of a few days, SL8). Hirose *et al.* (1999) identified the 1997 Bungo Channel silent earthquake (SL4) of M_{wa} 6.6 that had a source duration time of around 1 year and recurred in 2003 (SL9), as reported by GSI (2004). Recently, the Tokai silent earthquake (SL7) initiated in 2001 (Kimata *et al.*, 2002) and is still active with a current size of M_{wa} 7.0 (GSI, 2003b). All of the silent earthquakes were located between the subducting Philippine Sea and the over-riding Eurasian plates, except the two Offshore-Choshi silent earthquakes that recurred in 1999 (M_{wa} 5.6, source duration time of a few days, SL5) (Harada *et al.*, 2000) and in 2000

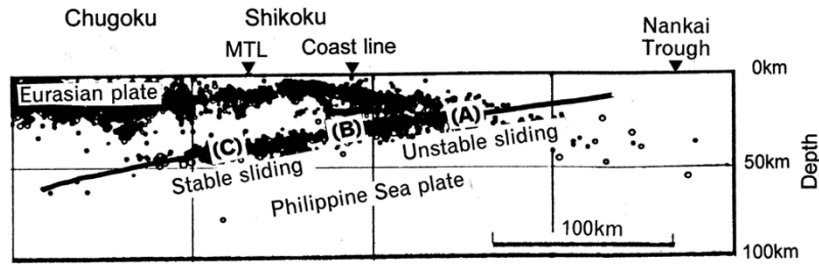


Fig. 1. Seismic cross section subparallel to the latitudinal line at longitude 133E across the Nankai Trough and Chugoku and Shikoku districts, where the Philippine Sea plate is subducting beneath the overriding Eurasian plate. MTL is median tectonic line. The area labeled (A) is the seismogenic region. (C) is a region where stable sliding on the subduction interface is dominant. (B) is the stable-unstable transition zone between (A) and (C). Modified from the panel E in figure 8 of Nakamura *et al.* (1997).

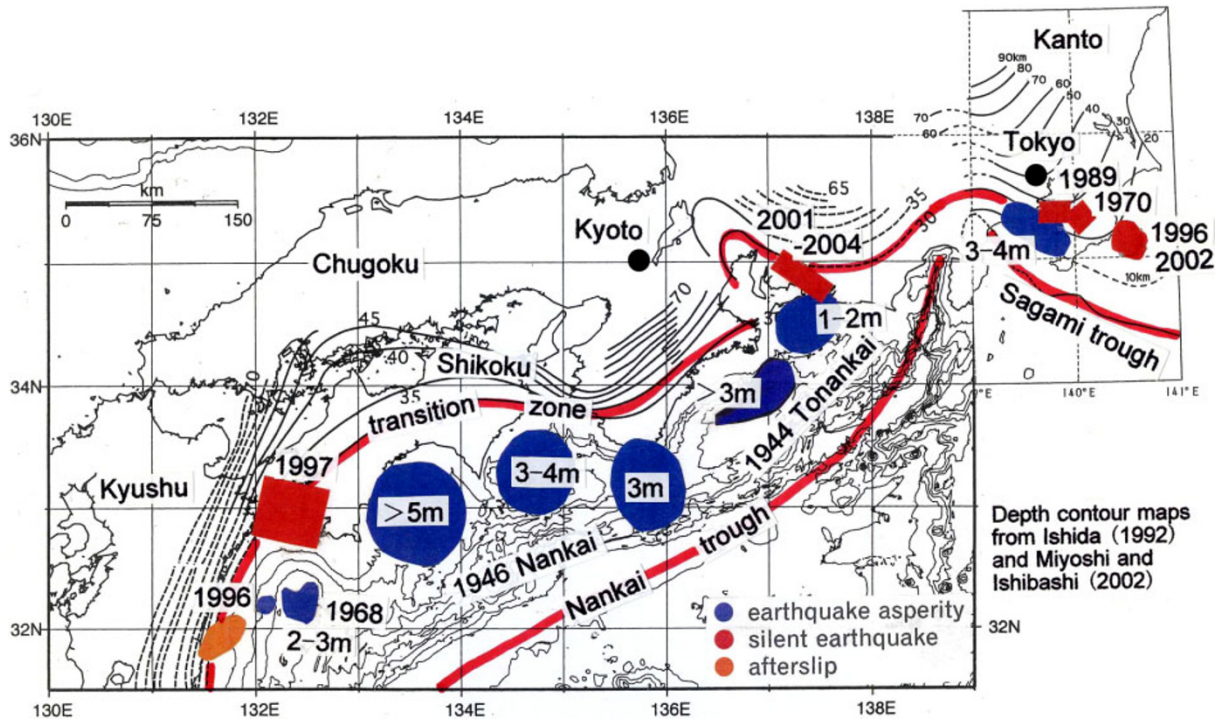


Fig. 2. Distribution of the silent earthquakes (solid), the afterslips (solid with course hatching) and major asperities (fine hatching) of M_w 8 class interplate earthquakes. Plate-depth contours are after Miyoshi and Ishibashi (2002) for southwest Japan including the Nankai Trough and Ishida (1992) for the Kanto district, including the Sagami Trough.

(M_w 5.6, source duration time of a few days, SL6) (Hirose *et al.*, 2001) on the subduction interface of the Pacific plate. It should be noted that the source duration time, T_0 , widely ranged from around 1 minute for the great M_w 8 earthquakes to a few years for the Tokai silent earthquake. Focal mechanisms of the slow-slip-events can be commonly interpreted to be low angle thrusting on the plate boundary. Seismic activity was generally not associated with these events, except for low level seismicity related to the two Boso Peninsula silent earthquakes (Sagiya, 2004). Obara (2002) discovered nonvolcanic deep tremors at depths of the stable-unstable transition zone, but their relation to the slow-slip-events is unknown.

Figure 2 shows the spatial distribution of the slow-slip-events and major asperities of the M_w 8 interplate earthquakes. Asperities of the 1923 Kanto and the 1944 Tonankai earthquakes were obtained by seismic waveform inversion by Wald and Somerville (1995) and Kikuchi *et al.* (2003),

respectively. Asperities of the 1946 Nankai earthquake are defined here as the areas which show large slips in all the inversion results obtained from leveling (Sagiya and Thatcher, 1999), tsunami (Tanioka and Satake, 2001) and seismic intensity data (Kanda *et al.*, 2003). Figure 2 displays that the slow-slip-events are separated from the major asperities. This kind of segregation was first reported by Yagi *et al.* (2001) for the asperity and the afterslip area of the 1996 Hyuganada earthquake. Average amount of slips of major asperities of the M_w 8 class earthquakes were around 3–5 m, except for the northeast smaller asperity of the Tonankai earthquake with a slip of 1–2 m. Average amounts of slips for the silent earthquakes were less than 0.2 m, one-order smaller than those of the major asperities. In other words, the silent earthquakes occurred in the transition zone between the seismogenic zone and the zone where stable sliding is dominant. The depth of the transition zone was suggested to be around 30 km along the Nankai Trough by thermal mod-

Table 1. Silent earthquakes, afterslips and Mw 8 class ordinary earthquakes along the Sagami and the Nankai Troughs. EQ1 to EQ3 are Mw 8 class giant earthquakes that occurred along the Sagami and the Nankai Troughs. SL1 to SL8 are silent earthquakes recently documented in Japan. AS1 and AS2 are afterslips. Mo and Moa are moments for ordinary and silent earthquakes, respectively. Mw is moment magnitude. Mwa is equivalent magnitude estimated from Moa through the relationship, $\log Moa = 1.5 \times Mw + 9.1$. Do is an overall slip. To is a source duration time. S, Leveling, Tilt and GPS in Data type column denote seismic records, levelling, continuous recording of crustal tilt, and GPS, respectively. References are (1) Wald and Somerville (1995), (2) Kikuchi *et al.* (2003), (3) Kanamori (1972), (4) Fujii (1993), (5) Hirose *et al.* (2000), (6) Sagiya (2004), (7) Hirose *et al.* (1999), (8) Harada *et al.* (2000), (9) Hirose *et al.* (2001), (10) GSI (2003b), (11) GSI (2003a), (12) GSI (2004) and (13) Yagi *et al.* (2001).

No.	Event	Mw	Mwa	Mo 10^{18} Nm	Moa	Do m	To day	Ref.	Data type
EQ1	1923 Kanto	7.9		700–800		3.5	0.0008	(1)	S
EQ2	1944 Tonankai	7.9		960		2.9	0.0007	(2)	S
EQ3	1946 Nankai	8.0		1500		3.1	0.001	(3)	S
SL1	1970 Chiba		6.5		7.6	0.4		(4)	Leveling
SL2	1989 Tokyo Bay		5.9		0.75	0.02	~1	(5)	Tilt
SL3	1996 Boso		6.0		1	0.1	~5	(6)	GPS
SL4	1997 Bungo Channel		6.6		11	0.18	~300	(7)	GPS
SL5	1999 Choshi-oki		5.6		0.33	0.03	~5	(8)	GPS
SL6	2000 Choshi-oki		6.1		1.7	0.17	2~3	(9)	GPS
SL7	2001-ongoing Tokai		7.0		40	0.20	~1500	(10)	GPS
SL8	2002 Boso		6.5		~10	0.1	~10	(11)	GPS
SL9	2003 Bungo-Channel		6.6		11	0.11	~60	(12)	GPS
AS1	1996 Hyuga-nada (a)		6.8		17	0.1	~50	(13)	GPS
AS2	1996 Hyuga-nada (b)		6.8		20	0.1	~50	(13)	jk,GPS

els (e.g., Hyndman and Wang, 1993) and geodetic inversions (e.g., Ito *et al.*, 1999).

3. A Source Parameter Gap between Ordinary and Silent Earthquakes

Figure 3 is a moment and moment-rate diagram. The fault length L is calculated using the relationship $Mo = 2 \times 10^6 \times L^3$ following Sato (1979), when plotting the iso- Vr lines in Fig. 3. It should be noted that there is a gap of 5 orders of moment rates between 10^{14} Nm/s of the silent earthquakes and 10^{19} Nm/s of the ordinary earthquakes as displayed in Fig. 3.

The zone between the two iso- Vr lines of 1 mm/s and 1 m/s (source duration times from days to years) is called the “GPS band” in this paper because all of the silent earthquakes in this zone were detected by GPS data. The other zone between 1 m/s and 1 km/s is hereafter called the “strainmeter and tiltmeter band” because the Tokyo Bay silent event (Hirose *et al.*, 2000) in this zone was detected by tiltmeter records.

There seem to be confusions on naming conventions of slow-slip-events. The present author would like to propose a new convention which names slow-slip-events in the strainmeter/tiltmeter band with source duration time of hours, “slow earthquakes” and events in the GPS band with source duration times of days to years, “silent earthquakes”. Also afterslips are not included as slow/silent earthquakes.

Table 2 shows the correspondence between the previous classification of slow-slip-events by Beroza and Jordan (1990), phases of the theoretical model of earthquake nucleation of Shibazaki and Matsu’ura (1998), some of the silent earthquakes and the new naming convention proposed. The fastest event among the silent earthquakes was the 1989 Tokyo Bay silent earthquake. Thus, there is a gap of 3 orders in rupture velocity between the silent earthquakes in the

Table 1 and the ordinary earthquakes and there were no slow-slip-events that accelerated to the “dynamic but slow rupture growth” of Shibazaki and Matsu’ura (1998).

4. Summary of Silent Earthquakes and Issues Related to Earthquake Prediction

We summarize below the basic features of the slow-slip-events along the Nankai and the Sagami Troughs detected to date.

(S1) There was a segregation between major asperities of Mw 8 class earthquakes and source areas of the slow-slip-events.

(S2) Major asperities of the Mw 8 class earthquakes were shallower than about 30 km in the seismogenic zone. Overall slips were about 3–5 m.

(S3) The silent earthquakes occurred in the stable-unstable transition zone at depths of around 30 km.

(S4) The silent earthquakes had Mwa less than 7 and overall slips were less than 0.2 m, one-order smaller than the major asperities of the ordinary Mw 8 earthquakes.

(S5) The silent earthquakes were associated with little seismic activity.

(S6) Moment release rates of the silent earthquakes along the Sagami Trough were one- or two-orders larger than those along the Nankai Trough.

(S7) There was a gap of 5-orders in the moment release rates between the silent earthquakes and the ordinary earthquakes. There were no slow earthquakes that reached the “dynamic but slow rupture growth”.

It is appropriate to mention ‘slow’ but seismic initial phases, as reported by Ellsworth and Beroza (1998). These observations could be described as slow-slip-events in their early stage, then seismically observable in their later stages as the seismic initial phase, if the forthcoming earthquake is large enough.

Table 2. Classification of slow-slip-events. Correspondence between classification of slow-slip-events by Beroza and Jordan (1990), phases of theoretical model of earthquake nucleation of Shibazaki and Matsu'ura (1998), some of silent earthquakes in Fig. 1 and naming convention proposed in this paper. V_r is rupture propagation velocity.

V_r	Beroza and Jordan (1990)	Shibazaki and Matsu'ura (1998)	Silent earthquakes	Naming proposed
1 km/s		dynamic rupture		—
0.1 km/s	slow eq.	dynamic but slow		slow eq.
10 m/s	silent eq.	rupture growth		
1 m/s			1989 Tokyo Bay	—
10 cm/s	creep event			
1 cm/s		quasi-static nucleation	1997 Bungo	silent eq.
1 mm/s			2001 Tokai	

Moment--Moment Rate diagram

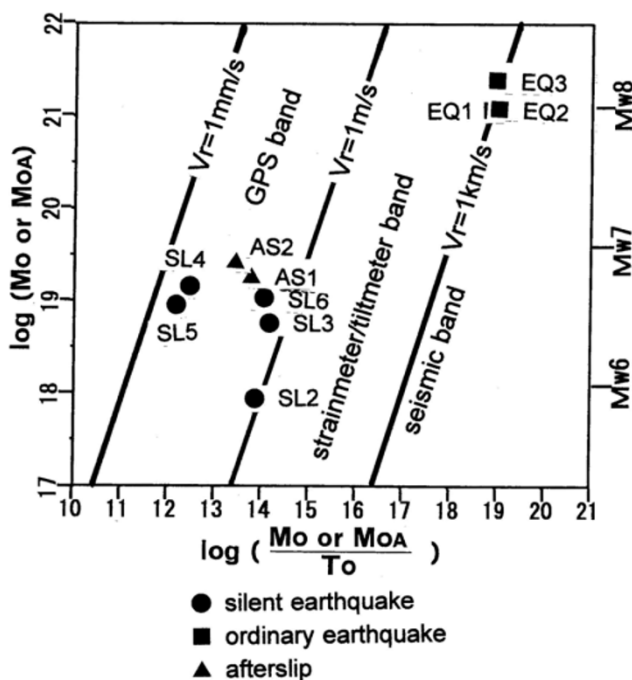


Fig. 3. Moment and moment-rate diagram. Vertical axis is static moment M_o or M_{oa} (Nm). Horizontal axis is moment rate (Nm/s), defined as M_o/T_o or M_{oa}/T_o , where T_o is overall source duration time. Diagonal lines are iso- V_r lines, where V_r is a characteristic rupture velocity. Circles denote silent earthquakes, triangles afterslips, and squares ordinary M_w 8 class earthquakes. See text for more details.

Studies of earthquake nucleation phase have been developed from laboratory experiments and numerical simulations based on constitutive laws of friction: e.g., Das and Scholz (1981), Dieterich (1979, 1986, 1994), Shibazaki and Matsu'ura (1998), Ohnaka and Shen (1999), and Kato and Hirasawa (1999). The rate- and state-dependent friction law is now widely accepted. Although several variations of the friction law were proposed, the friction parameter, a - b , in the so-called Dieterich-Ruina law is commonly used to describe quasi-static nucleation processes.

Yoshida and Kato (2003) and Kato (2003) performed numerical simulations of two block models having different friction. Following their results, we could regard silent earthquakes as one of the episodic phases in the stable-unstable

transition zone in the later stage of the seismic cycle.

Thus, the following issues are raised which are associated with earthquake prediction.

(Issue-1) Do slow earthquakes occur with M_w 7 or greater and shorter source duration time of hours, filling the gap in (S7)? In other words, what is the link between the silent earthquakes in the stable-unstable transition zone and ordinary earthquakes in the seismogenic zone?

(Issue-2) Could we anticipate how silent earthquakes will grow?

5. Empirical Source Time Function based on Laboratory Experiments

Ohnaka and Shen (1999) carried out laboratory experiments on fault failure under compression on preexisting faults having different roughness. The earthquake nucleation phase consisted of three subphases, a quasi-static phase, an accelerating phase and a fast-speed dynamic rupture. The stage between the accelerating phase and the fast-speed dynamic rupture is called the critical stage.

Depending on the roughness of the fault surfaces, nucleation processes were quite different. In the case of a rough fault, growth rate was small and it took a long time to reach dynamic rupture, while growth rate was large for a smooth fault. However, they showed that, normalizing $\ln(t)$ (size of nucleation zone) to λc (the roughness of fault surface, see Ohnaka and Shen, 1999), growth rate $V_n(t)$ during the accelerating phase obeys a single comprehensive power law as

$$\frac{V_n(t)}{V_s} = 8.87 \times 10^{-29} \times \left(\frac{\ln(t)}{2\lambda c} \right)^{NK} \quad (1)$$

where $NK = 7.31$ and V_s is the S-wave velocity. The subscript n denotes a quantity during the accelerating phase. It should be noted that the exponent NK and the proportionality constant 8.87×10^{-29} varies with stiffness, normal stress and stress rate and thus discussions below should be regarded as a zero-order approximation.

A fault parameter linearly related to geodetic observations is the moment, $M_{on}(t)$ (Nm), of the nucleation zone. We would like to transform Eq. (1) to a differential equation for $M_{on}(t)$. For this purpose, we begin by deriving another power law which relates $\ln(t)$ to $M_{on}(t)$ as below.

Ohnaka (2000) suggested relationships between seismic moment M_o , critical distance D_c and critical length L_c as

$$M_o = 10^{19} \times D_c^3 \quad (2)$$

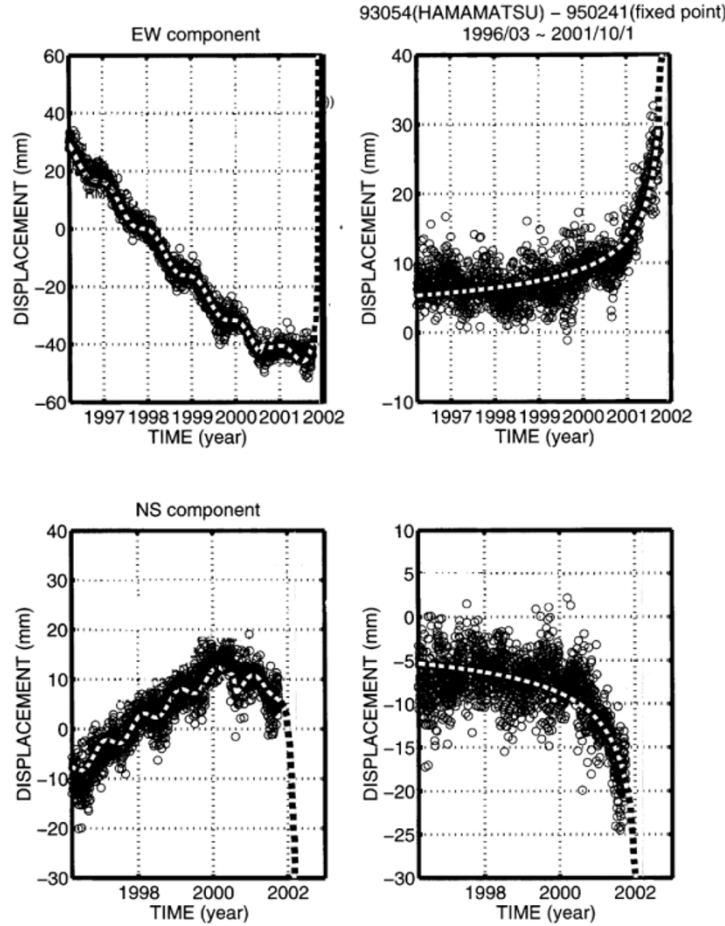


Fig. 4. EW (upper figure) and NS (lower) components of GPS horizontal displacements at Hamamatsu due to the Tokai silent earthquake (SL7 in Table 1). Vertical axis is the GPS displacement. Horizontal axis is time in years. Dots are daily values. Graphs on the left are original data. Graphs on the right show data with linear trends and annual variations removed. Broken lines are fitted curves for the period of 1996–2001 based on the time-to-failure analysis of Kawamura *et al.* (2002).

$$M_o = 10^9 \times L_c^3 \quad (3)$$

where the units of proportionality coefficients are N/m^2 . Note that L_c is the size of the nucleation zone at the critical stage in this paper but was its half length in Ohnaka and Shen (1999). The subscript c denotes a quantity at the critical stage. Squaring both sides of (3), multiplying by (2) and taking the cube root, we have $M_o = 10^{1/3} \times 10^{12} \times D_c \times L_c^2$. Assuming W_c (width of nucleation zone) = L_c and μ (rigidity) = $4 \times 10^{10} \text{ N/m}^2$, we have the moment at the critical stage as $M_{oc} = \mu \times L_c \times W_c \times D_c = 4 \times 10^{10} \times L_c^2 \times D_c$. Then, we have

$$M_{oc} = 2 \times 10^7 \times L_c^3. \quad (4)$$

Assuming the same relationship as Eq. (4) for the accelerating phase to replace M_{oc} and L_c with $Mon(t)$ and $Ln(t)$, we have the second power law as

$$Mon(t) = 2 \times 10^7 \times Ln(t)^3. \quad (5)$$

The proportionality coefficient of $2 \times 10^7 \text{ (N/m}^2)$ is one-order larger than that for ordinary earthquakes (e.g., Sato, 1979). Equation (5) is rewritten as

$$Ln(t) = g \times Mon(t)^{1/3} \quad (6)$$

where $g = (2 \times 10^7)^{-1/3}$. Substituting $Ln(t)$ in Eq. (6) into Eq. (1), we have

$$Vn(t) = h \times Mon(t)^{NK/3} \quad (7)$$

where $h = 8.87 \times 10^{-29} \times V_s \times [g/(2\lambda c)]^{NK}$.

The nucleation zone expands by $dLn(t) = Vn(t)dt$ during a time increment dt . Substituting (6) and (7) into $dLn(t) = Vn(t)dt$, we have

$$dt = \frac{dLn(t)}{Vn(t)} = \frac{dMon(t)}{q \times Mon(t)^{(NK+2)/3}} \quad (8)$$

where $q = (3h/g) = 3 \times 8.87 \times 10^{-29} \times V_s \times g^{NK-1}/(2\lambda c)^{NK}$. From (8), we have the following ordinary differential equation as

$$\frac{dMon(t)}{dt} = q \times Mon(t)^{(NK+2)/3} \quad (9)$$

assuming that $(NK + 2)/3$ and $Mon(t)$ are larger than 0. Equation (9) describes growth during the accelerating phase.

Integrating (8) from t to t_d , we have

$$t = t_d - T_E(t) \quad (10)$$

where t_d is the time when $Mon(t_d)$ is infinite and

$$T_E(t) = \frac{3}{q \times (NK - 1) \times Mon(t)^{(NK-1)/3}}. \quad (11)$$

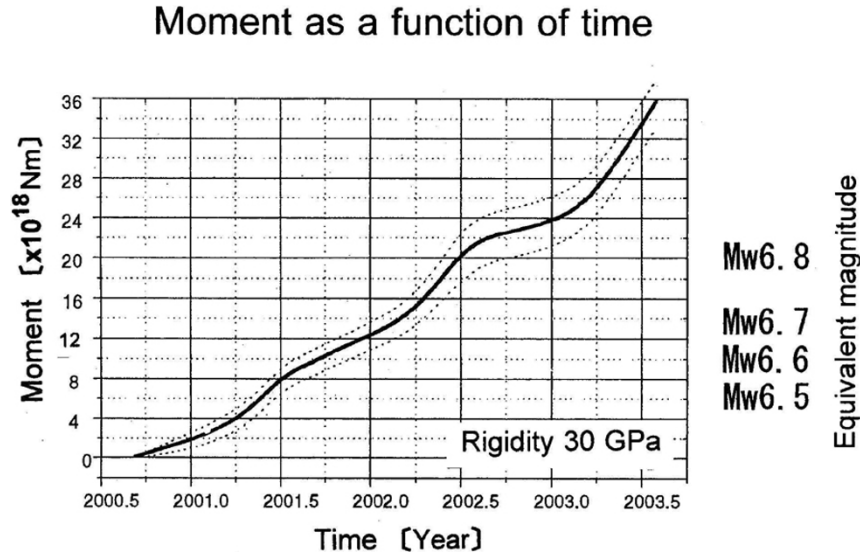


Fig. 5. Solid line is the moment of the Tokai silent earthquake as a function of time for the period from 2000 to 2003, modified from GSI (2003b). Broken lines show a width of one standard deviation. Horizontal axis is years. Vertical axis is (left) static moment Moa and (right) its equivalent magnitude.

It should be noted that q is inversely proportional to λc^{NK} and then $T_E(t)$ is proportional to λc^{NK} .

Solving (10) and (11), we have

$$Mon(t) = \frac{Mon(t_0)}{[1 - (t - t_0)/T_E(t_0)]^{3/(NK-1)}} \quad (12)$$

where t_0 is a reference time and $t_d - t_0 = T_E(t_0)$. The exponent of $3/(NK - 1)$ is around 1/2 since $NK = 7.31$ for the laboratory experiment of Ohnaka and Shen (1999). Equation (12) seems to be consistent with overall waveforms suggested by previous laboratory experiments and numerical simulations (e.g., figure 6 in Dieterich, 1986).

6. Application of the Empirical Source Moment Function

We try to fit synthetic waveforms using the source moment function of Eq. (12) to waveforms from silent earthquakes. This is quite similar to the time-to-failure analysis with an exponent of around -1 by Varnes (1989) and Main (1999) for predicting failure using seismicity prior to main shocks and volcanic eruptions.

The Tokai silent earthquake was first detected and observed to accelerate during the first half of 2001. Figure 4 shows the EW (upper figure) and the NS (lower) components of the GPS horizontal displacements at Hamamatsu. Broken lines are fitted curves for the period of 1996–2001 based on the time-to-failure analysis of Kawamura *et al.* (2002), suggesting a failure at the end of 2001 or beginning of 2002. However, the event decelerated in the last half of 2001 and again accelerated in the first half of 2002, and now the Mwa of the event has grown larger than Mwa 7.0, as illustrated in Fig. 5, which shows the moment of the Tokai silent earthquake as a function of time for the period from 2000 to 2003 (GSI, 2003b).

This analysis tells us that a single cycle of rupture growth process can be modeled with the source moment function (Eq. (12)) but the whole process including accelerations and deceleration can not be adequately modeled. This implies

that the whole process is dependent on the heterogeneous distribution of the frictional properties and a quantitative prediction based on a fault constitutive relations requires proper numerical mapping of the frictional properties.

7. Estimate of Roughness of the Subduction Interface

We try to give order of magnitude estimates of the fault roughness by fitting synthetic displacements to observed waveforms of two recorded silent earthquakes.

Figure 6(A) shows GPS horizontal displacements due to the 1997 Bungo Channel silent earthquake (SL4). Vertical lines (E1)–(E5) indicate five earthquakes of Mw 5.8–6.7 which occurred in 1997 and 1998 in and around Kyushu Island. The silent earthquake was separated in space and time from these earthquakes (Hirose *et al.*, 1999; Ozawa *et al.*, 2001). Comparing the synthetic displacements in Fig. 6(B) with observed data at Saiki and Misho in (A), it can be concluded that there is a fair agreement for λc from 5 m to 8 m and a satisfactory fit for $\lambda c = 6.5$ m in the time window from (b) to (c).

Comparing synthetic crustal tilts to the observed data at Aikawa (AKW, borehole depth 95 m), Fuchu (FCH, 2750 m) and Iwatsuki (IWT, 3510 m), we can obtain an order of magnitude estimate of $\lambda c = 2 \pm 0.5$ m for the source area of the 1989 Tokyo Bay silent earthquake (SL2).

We would like to emphasize that this is a unique way to estimate the roughness of subduction interface.

The stable-unstable transition zone corresponds to a boundary zone where $|a-b|$ is small between the seismogenic zone where velocity weakening ($a-b < 0$) dominates and the stable sliding zone where velocity hardening ($a-b > 0$) dominates. Based on numerical simulations of a two-degree-of-freedom block-spring model, Yoshida and Kato (2003) showed that slow-slip-events could occur where $|a-b|$ is small. Thus, the long source duration times of the silent earthquakes could be due to the small $|a-b|$ of the stable-unstable transition zone.

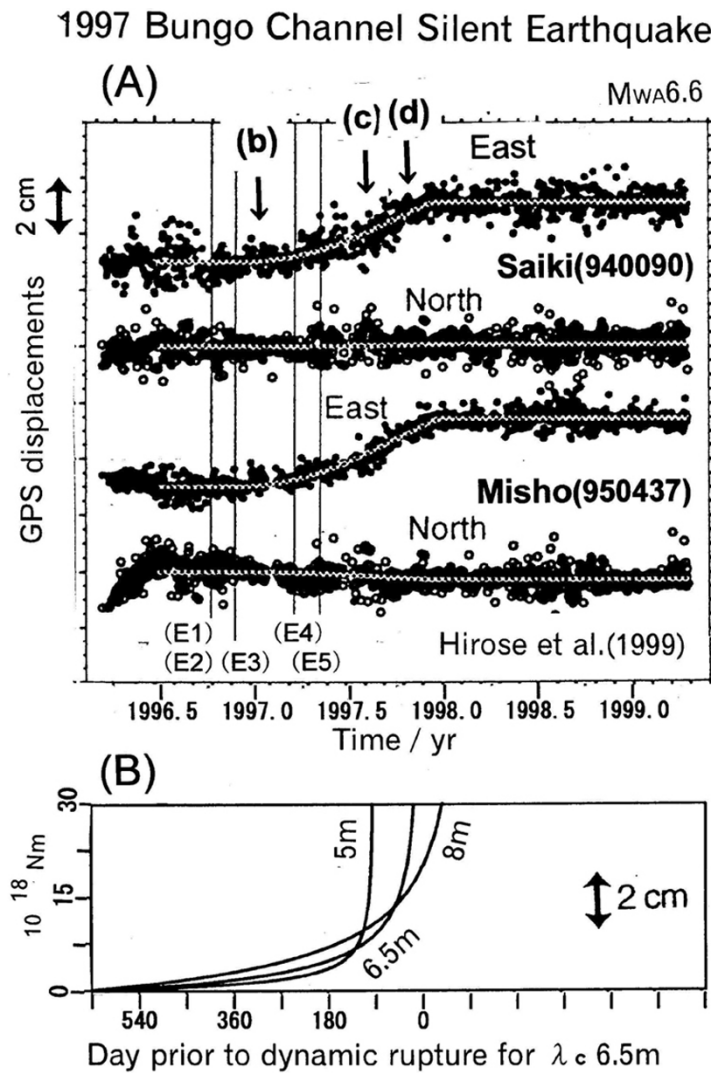


Fig. 6. (A) GPS horizontal displacements at Saiki (32.92N, 131.88E) on Kyushu Island and Misho (32.96N, 132.56E) on Shikoku Island in southwest Japan. Horizontal axis is time in years. Vertical axis is displacement in cm. Vertical lines indicate earthquakes on (E1) Oct. 18, 1996 (M_w 6.6, 30.47N, 131.29E, Depth 22 km), (E2) Oct. 19, 1996 (M_w 6.7, 31.78N, 131.78E, Depth 22 km), (E3) Dec. 02, 1996 (M_w 6.7, 31.76N, 131.72E, Depth 33 km), (E4) May 13, 1997 (M_w 6.0, 32.00N, 130.26W, Depth 16 km) and (E5) June 25, 1998 (M_w 5.8, 34.43N, 131.35E, Depth 15 km). (b), (c) and (d) denote times when the nucleation phase was suggested to be initiated, decelerated and arrested, respectively. Modified from Hirose *et al.* (1999). (B) shows synthetic source moment $Mon(t)$ at Misho for λ_c of 5 m, 6.5 m and 8 m. Vertical axis is moment in Nm, which is scaled to surface displacement at Misho.

8. Estimate of the Magnitude of $a-b$

We attempt another way to give a numerical estimate of the friction. Dieterich (1992) and Kato (2003) derived relationships between the size of a silent earthquake and the friction parameter $a-b$ from the Dieterich-Ruina law as

$$a-b = -c\mu Ls / (rc \times \sigma n) \quad (13)$$

where rc is the radius of a circular area of a silent earthquake, μ is rigidity, Ls is a characteristic slip, σn is normal stress, and $c = 7\pi/24$. A major difficulty is that the values of σn and Ls are unknown. Here, we tentatively assume that σn is equal to the lithostatic stress. If the slip of a silent earthquake becomes larger than Dc , it becomes a dynamic rupture. Thus, the slip of a silent earthquake should be less than Dc , which gives a lower bound of Dc . Here the slip of a silent earthquake is tentatively assumed to be equal to the characteristic slip Dc . If we assume $Dc/Ls = 10$ following Kuwahara *et al.* (1987), Ls can be assumed to be one-tenth

Table 3. Numerical estimate of friction parameter $a-b$. rc is a radius of a circular area of a silent earthquake, which is assumed here to be a squared root of a faulting area over π . μ is rigidity, Ls characteristic slip, σn normal stress, and $c = 7\pi/24$.

	rc km	μ 10^{10} Nm	Ls cm	σn MPa	$a-b$ 10^{-5}
SL2	9.1	4	0.24	900	-10
SL4	33.9	4	1.8	600	-3
SL7	25.9	3	2.0	600	-3

of the slip of a silent earthquake. With Eq. (13) and these assumptions, we can obtain an order of magnitude estimates of $a-b$ as in Table 3. Considering the assumptions above, the numerical estimates should be regarded as lower limits of $|a-b|$.

The values are two-orders smaller than those determined

from laboratory slip experiments (e.g., Kato and Hirasawa, 1999), which is consistent with the conclusion by numerical simulation of Yoshida and Kato (2003) suggesting that slow-slip-events are liable to occur where $|a-b|$ is small.

9. Concluding Remarks

Major features of the slow-slip-events along the Nankai and the Sagami Troughs can be summarized as follows: There was a segregation between major asperities of M_w 8 class earthquakes and source areas of the slow-slip-events. Silent earthquakes occurred in the stable-unstable transition zone at depths of around 30 km. Overall slips were less than 0.2 m, one-order smaller than major asperities. There was a gap of 5-orders in the moment rates between the silent earthquakes and the M_w 8 class ordinary earthquakes.

One problem in using these ideas for the prediction of great subduction zone earthquakes using numerical simulations based on constitutive laws of friction with distribution of the interplate friction is that there is not sufficient information to numerically map the heterogeneous distribution of friction. Two methodologies are attempted to obtain order of magnitude estimates of the roughness and the friction parameter in the source areas of the silent earthquakes. One method compares observed data to synthetic waveforms with a source time function described by Eq. (12). The other relates sizes of silent earthquakes to $a-b$, based on Eq. (13). However, the numerical estimations do not include sufficient information on the level of friction. These estimates should be regarded as a starting point toward future development of numerical mapping of the interplate friction.

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